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Continuum Fatigue Damage Modeling for Use in Life Extending Control

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Abstract

This paper develops a simplified continuum (continuous wrp to time, stress, etc.) fatigue damage model for use in Life Extending Controls (LEC) studies. The work is based on zero mean stress local strain cyclic damage modeling. New nonlinear explicit equation forms of cyclic damage in terms of stress amplitude are derived to facilitate the continuum modeling. Stress based continuum models are derived. Extension to plastic strain-strain rate models are also presented. Application of these models to LEC applications is considered. Progress toward a non-zero mean stress based continuum model is presented. Also, new nonlinear explicit equation forms in terms of stress amplitude are also derived for this case.

I. Introduction

A strong motivation for the current activities to develop continuum fatigue damage models comes from the ongoing work in the areas of life extending and or damage mitigating controls (refs. 1 to 3, respectively). These controls studies seek to create control methodologies to allow the reduction of damage in critical components in aerospace systems by the manner in which the control moves the system transiently between setpoints. The transient damage for critical components in rocket engines has been shown to be capable of reductions on the order of 2/3, by the manner in which the control moves the engine through the transient. This has been accomplished without significant loss in dynamic response (ref. 4). The results quoted above are based on open-loop studies which have been accomplished through the use of gross nonlinear optimization. The continued development of life-extending control requires a damage model which is continuum based, as opposed to current fatigue damage models which are cyclic extrema based. Contemporary cyclic methods require a completed stress strain cycle before the associated damage can be determined. What is required for controls is the ability to predict for the next increment, or continuum, of stress or strain what the associated fatigue damage will be. That is the thrust of this paper. Clearly it is desirable to create as simple a continuum model as possible, since this will allow a more broad application of the life extending control concepts. Only very limited work has been done in this area. The initial work done by A. Ray et al. at Penn State University (ref. 5) has created a useable continuum model for fatigue damage. However, this model is hindered by the requirement of identifying the cycle extrema and then calculating the damage between the extrema based on extrema information. This complicates considerably the use of such a model in a practical control design. It requires a continuous accounting of the cycle extrema and the changing (bookkeeping) of these extrema as the physics of the process progresses. An approach which would use only local stress or strain to infer damage would be simpler and hence superior.

This paper seeks to create a zero mean stress continuum fatigue damage model in two forms, the first form is stress based and the second is plastic strain and strain rate based. The paper introduces new simplified forms for the cyclic damage results, for the zero mean stress case. Progress on a non zero mean stress continuum model is also shown and the open issues that remain in this area are discussed.

The basic objective of this work is to generate a damage model for the fatigue failure of metallic materials which is continuum or differential based as opposed to current theory which is cycle based. The fundamental approach of the paper is to use results from the cyclic local strain method as a basis for the development of the continuum model. The next section will present a short summary on those parts of the local strain approach required for the material which follows. The work of Dowling et al. (ref. 6) will be the focal point that will be used in this paper as the basis of the local strain method.

Local Strain Method

The basis of current damage (fatigue/fracture) approaches, study the experimental results of applying cyclic loads of various amplitude and various mean (constant) bias loads, and summarize/generalize these to allow prediction of arbitrary combinations of loading cycles. Many variations and methods have been evolved. A fairly straight forward approach (called the local strain approach) by Dowling et al. (ref. 6) will be the foundation for the analysis which follows.

A typical stress-strain hysteresis loop is shown in figure 1(a). The effect of cycle amplitude changes (with zero mean stress) is illustrated in figure 1(b). The back bone plot (cyclic stress-strain curve) which is the locus of the extrema of the stress-strain cycles is shown (ref. 6) to have the mathematical form (for materials of interest);

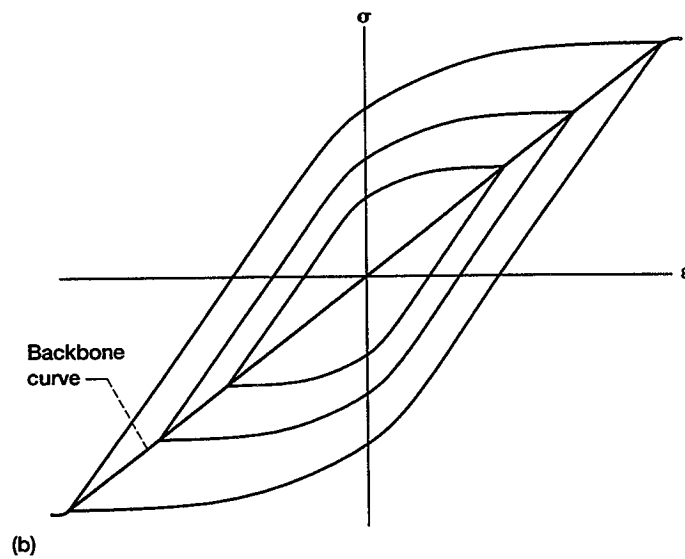
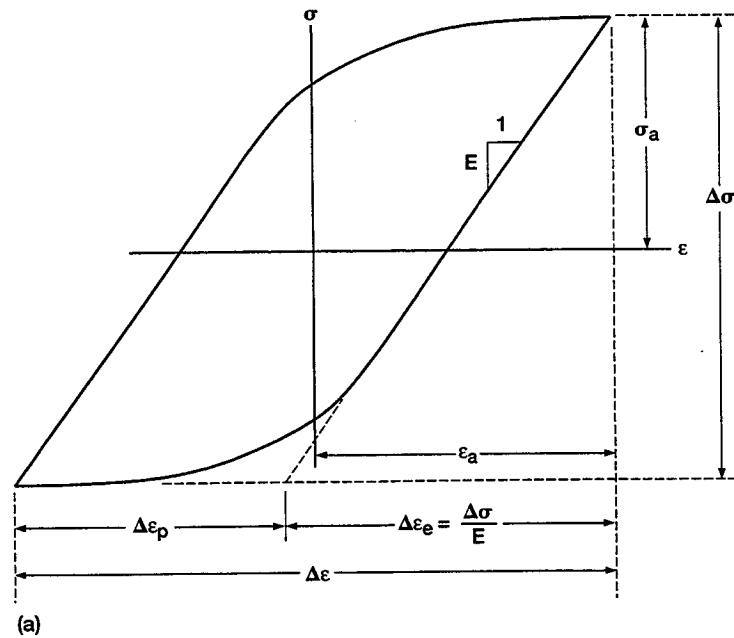


Figure 1.—Cyclic stress-strain. (a) Typical hysteresis loop. (b) Stress-strain cycles of various amplitudes—with backbone curve.

$$\epsilon_a = \frac{\sigma_a}{E} + \left(\frac{\sigma_a}{A} \right)^{1/s} \quad (1)$$

where $\epsilon_a = \Delta\epsilon/2$ and $\sigma_a = \Delta\sigma/2$ are strain and stress amplitude, respectively, and E , A , and s are material constants. The cyclic damage associated with repeated hysteresis stress-strain cycles of a given amplitude is determined by experimental observation to have the mathematical form:

$$\epsilon_a = \frac{\sigma'_f}{E} (2N_f)^b + \epsilon'_f (2N_f)^c \quad (2)$$

where b , c , E , σ'_f and ϵ'_f are constants for a particular material and N_f is the number of cycles to failure. The plot of figure 2 shows a typical curve as described by equation (2).

The total strain amplitude (eq. (1)) is seen to be composed of two parts the elastic strain contribution.

$$\epsilon_{a_e} = \frac{\sigma_a}{E} = \frac{\sigma'_f}{E} (2N_f)^b \quad (3)$$

and the plastic strain contribution

$$\epsilon_{a_p} = \left(\frac{\sigma_a}{A} \right)^{1/s} = \epsilon'_f (2N_f)^c \quad (4)$$

Equation (2) now can be used to estimate the damage associated with a cycle of strain of amplitude ϵ_a . Since N_f is the number of cycles to failure at amplitude ϵ_a then $1/N_f$ is the damage of a single cycle (assuming no effect of accumulated damage). Therefore n cycles of amplitude σ_a will create a damage D of

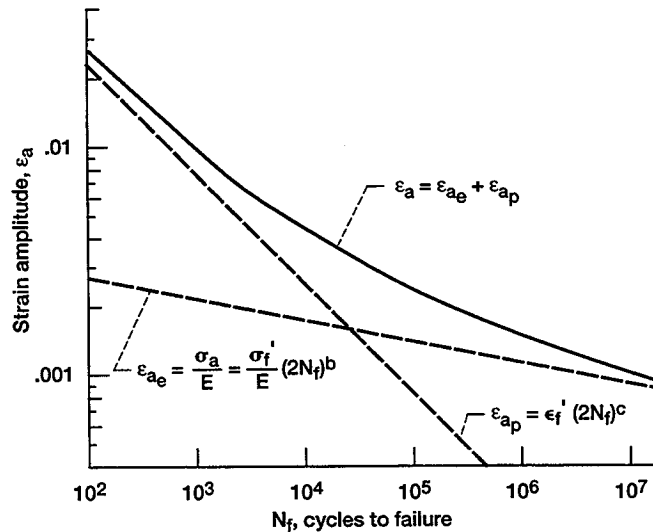


Figure 2.—Cycles to failure versus strain amplitude.

$$D = \frac{n}{N_f} \quad (5)$$

where $D = 1$ represents failure. Then the Palmgren-Miner equation may be used to determine the damage for cycles of different amplitudes, i.e.

$$D = \sum_i \frac{n_i}{N_{fi}} \quad (6)$$

where i represents the various amplitudes composing the strain history. Various corrections can be applied for the effect of mean stress superimposed on the cycles and alternate methods have been evolved to account for the effect of damage accumulation (nonlinearity) on the damage of any particular cycle.

Zero Mean Stress Continuum Damage Model

Because of the strong nonlinear terms in equations (1) and (2) above, these equation forms are not directly suitable for the continuum model development. Fortunately, there is a redundancy in the material properties ($b, c, E, \sigma'_f, \epsilon'_f$, and s) that can be used. This can be determined from equations (3) and (4) by solving for $2N_f$ in each and eliminating $2N_f$. Thus

$$\epsilon_{p_a} = \epsilon'_f \left(\frac{\sigma_a}{\sigma'_f} \right)^{c/b} \quad (7)$$

where ϵ_{p_a} is the amplitude of the plastic strain.

Now using $(\sigma_a/A)^{1/s}$ to eliminate ϵ_{p_a} and rewriting the right hand side of equation (7) gives

$$\left(\frac{\sigma_a}{A} \right)^{1/s} = \left[\frac{\sigma_a}{\sigma'_f} (\epsilon'_f)^{b/c} \right]^{c/b} \quad (8)$$

For this to be true the following must apply

$$\frac{1}{s} = \frac{c}{b} \quad (9)$$

and

$$A \epsilon_f'^{b/c} = A \epsilon_f'^s = \sigma'_f \quad (10)$$

For the materials study in reference 6, these relationships are found to be virtually exact for RQC-100 and approximately correct for MAN-TEN steel. These equations are assumed to be generally approximately correct for many metallic materials and will be used in the analysis which follows.

In the analysis that follows stress, σ , will be considered as the independent variable. While it is true that in typical fatigue testing the strain amplitude is held constant, it also seems clear by analogy to fluid and current flow and other physical processes that load or potential (stress) is the cause of motion (strain in this case). Therefore, equations (1) and (2) will be combined eliminating the strain amplitude ϵ_a , thus

$$\epsilon_a = \frac{\sigma_a}{E} + \left(\frac{\sigma_a}{A} \right)^{1/s} = \frac{\sigma'_f}{E} (2N_f)^b + \epsilon'_f (2N_f)^c \quad (11)$$

or since $\delta_{cyc} = 1/N_f$, where δ_{cyc} is the damage per cycle this can be written as

$$\epsilon_a = \frac{\sigma_a}{E} + \left(\frac{\sigma_a}{A} \right)^{1/s} = \frac{\sigma'_f}{E} \left(\frac{\delta_{cyc}}{2} \right)^{-b} + \epsilon'_f \left(\frac{\delta_{cyc}}{2} \right)^{-c} \quad (12)$$

The elastic terms and the plastic terms in equation (12) are now considered separately to determine δ_{cyc} . For the elastic terms,

$$\frac{\sigma_a}{E} = \frac{\sigma'_f}{E} \left(\frac{\delta_{cyc_e}}{2} \right)^{-b} \quad (13a)$$

yields

$$\delta_{cyc_e} = 2 \left(\frac{\sigma_a}{\sigma'_f} \right)^{-1/b} \quad (13b)$$

For the plastic terms

$$\left(\frac{\sigma_a}{A} \right)^{1/s} = \epsilon'_f \left(\frac{\delta_{cyc_p}}{2} \right)^{-c} \quad (14a)$$

yields

$$\delta_{cyc_p} = 2 \left(\frac{1}{\epsilon'_f} \right)^{-1/c} \left(\frac{\sigma_a}{A} \right)^{-1/cs} = 2 \sigma_a^{-1/cs} \left(\frac{1}{A \epsilon_f'^s} \right)^{-1/cs} \quad (14b)$$

Using the material relations of equations (9) and (10), the damage per cycle for the plastic part of equation (12) becomes

$$\delta_{cyc_p} = 2 \left(\frac{\sigma_a}{\sigma'_f} \right)^{-1/b} \quad (14c)$$

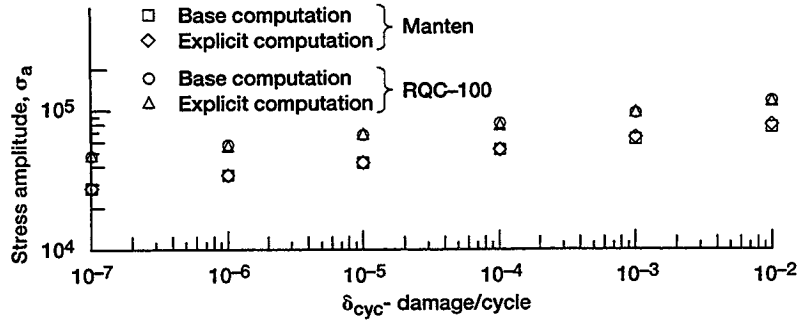


Figure 3.—Damage per cycle, δ_{cyc} versus stress amplitude σ_a , for Manten and RQC-100 steels; for base computation (EQ 12) and explicit computation (EQ 15).

Now since equations (13b) and (14c) are the same and satisfy both parts of equation (12), it is the solution (restatement) of equation (12). Thus, the zero mean stress case cyclic damage law can be written.

$$\delta_{cyc} = 2 \left(\frac{\sigma_a}{\sigma'_f} \right)^{-1/b} \quad (15a)$$

or

$$N_f = \frac{1}{2} \left(\frac{\sigma_a}{\sigma'_f} \right)^{1/b} \quad (15b)$$

These equations represent the average (or midlife) damage/cycle in terms of the stress amplitude (at midlife) for strain controlled cyclic fatigue. To validate this result against data, the ϵ_a versus N_f life results for RQC-100 and MANTEN steels (ref. 6) were used as a test case. To do this equation (12) was solved numerically for σ_a versus δ_{cyc} and compared to the results of equation (15), figure 3. The results appear to be within the accuracy of the numerical solutions over five decades of δ_{cyc} . The explicit form of equation (15) now allows further analysis toward a continuum damage model.

With stress as the independent variable driving damage and knowing the damage per cycle (eq. (15)) then

$$\int_{cycle} \delta'(\sigma) d\sigma = \delta_{cyc} = 2 \left(\frac{\sigma_a}{\sigma'_f} \right)^{-1/b} \quad (16)$$

where $\delta'(\sigma)$ is the damage rate $\delta'(\sigma) = d\delta/d\sigma$ as the cycle is transversed. Now a critical question is; over which part of the cycle does the damage occur. Various assumptions are possible, with reference to figure 4. It is plausible that damage is not likely generated during the relaxation (unloading) phases of the cycle, namely $A \rightarrow B$ and $C \rightarrow D$, although cracks and acoustic emissions may be observed. Damage is most likely during tensile stressing $D \rightarrow A$ and may also occur during compressive stressing $B \rightarrow C$.

The initial assumption will be that damage occurs only for $\sigma > 0$ and σ increasing (domain $D \rightarrow A$, fig. 4), again assuming linear damage accumulation then

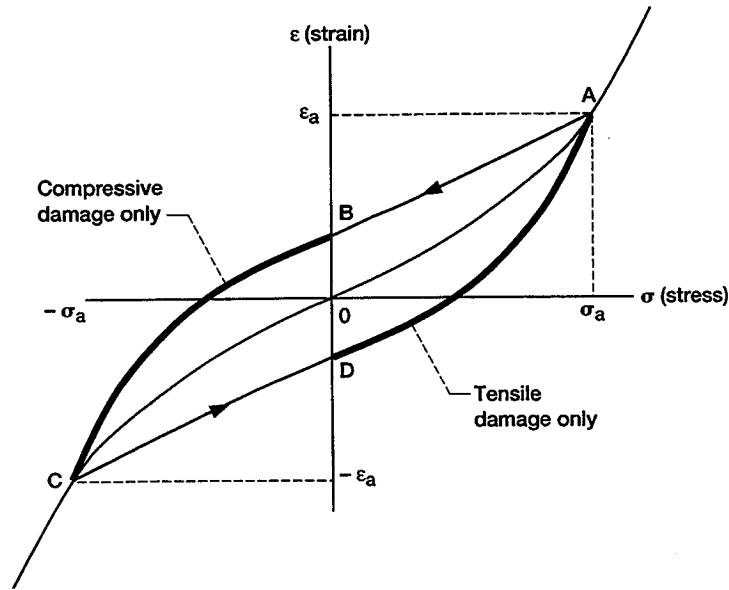


Figure 4.—Assumed damage producing domains.

$$\int_0^{\sigma_a} \delta'(\sigma) d\sigma = \delta_{cyc} = 2 \left(\frac{\sigma_a}{\sigma'_f} \right)^{-1/b} \quad (17)$$

It is readily shown that

$$\delta'(\sigma) = -\frac{2}{b\sigma'_f} \left(\frac{\sigma}{\sigma'_f} \right)^{-(1+b)/b} \quad (18a)$$

or

$$\delta'(\sigma) = \frac{-2}{b\sigma'_f} \left(\frac{|\sigma|}{\sigma'_f} \right)^{-(1+b)/b} \quad (18b)$$

also works. Thus the rate at which damage accumulates over the cycle is given by equation (18). This result is extremely nonlinear, for example for RQC-100 steel, $b = 0.075$, $\sigma'_f = 1.68 \times 10^5$ is

$$\delta'(\sigma) = 1.5872 \times 10^{-4} \left(\frac{\sigma}{1.68 \times 10^5} \right)^{12.3333} \quad (18d)$$

This form shows the extreme sensitivity to small changes (and errors) in stress. It is important to note that equation (18) is independent of cycle amplitude, i.e., applies to any zero mean stress cycle. Also equation (18) does not depend on knowledge of the cycle extrema (reference values). A plot of equation (18) for RQC-100 steel is presented in figure 5(a). Figure 5(b) shows the damage rate location in a cycle.

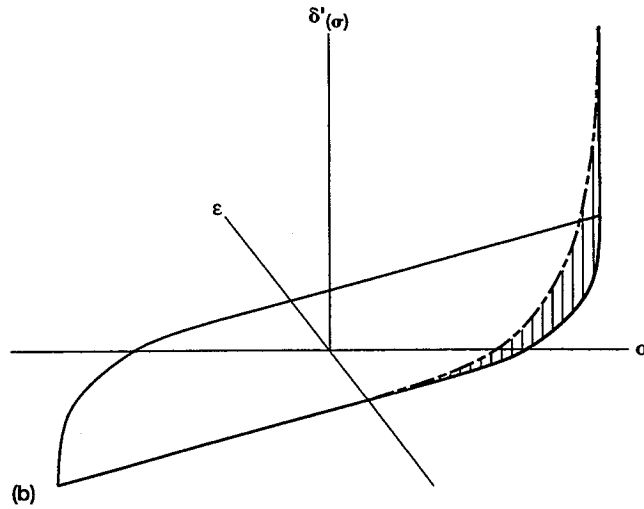
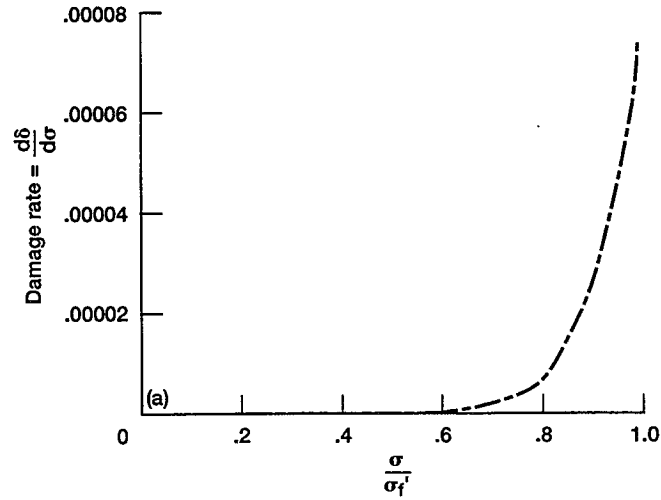


Figure 5.—Damage rate versus stress. (a) RQC-100 steel.
(b) Location on hysteresis cycle.

If damage occurs equally in tension and compression then

$$\delta'(\sigma) = -\frac{1}{b\sigma_f'} \left(\frac{|\sigma|}{\sigma_f'} \right)^{-(1+b)/b} \quad (19)$$

applies over domain $B \rightarrow C$ and $D \rightarrow A$ in figure 4. In view of the mean stress effect on damage, it is more likely that greater damage occurs, over the domain $D \rightarrow A$ than $B \rightarrow C$, therefore an unequal damage distribution such as

$$\delta'(\sigma) = \begin{cases} -\frac{2k}{b\sigma_f'} \left(\frac{|\sigma|}{\sigma_f'} \right)^{-(1+b)/b} & \text{for } \sigma > 0, \sigma \text{ increasing} \\ -\frac{2(1-k)}{b\sigma_f'} \left(\frac{|\sigma|}{\sigma_f'} \right)^{-(1+b)/b} & \text{for } \sigma < 0, \sigma \text{ decreasing} \end{cases} \quad (20)$$

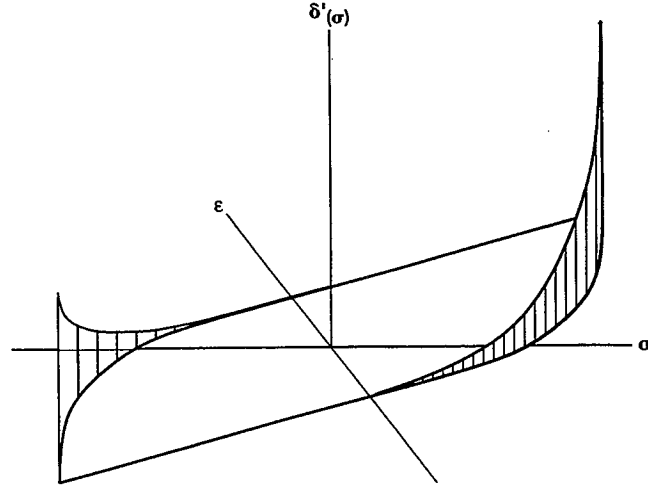


Figure 6.—Damage rate distribution for combined tensile and compressive damage.

may be a more likely scenario than the equal damage case equation (19). In this equation the parameter k , weights the tension side damage relative to the compressive side. Figure 6 illustrates the damage distribution for this case.

Any of the above forms (eqs. (18) to (20)), can be used as a basis for damage estimation for Life Extending or Damage Mitigating Control. These forms are particularly useful because they depend only on stress (and material constants), which can be estimated from associated structural models. Clearly the case represented by equation (20), is the most general form containing the other two by proper selection of k . However the case of equation (18) shows the simplicity of the approach and is easily used to derive further results which may then be generalized.

To convert the above results to a model useable in the time domain, the case with damage occurring only with increasing tensile load (eq. (18)) will be considered.

For this case the damage rate is given by:

$$\delta'(\sigma) = \frac{d\delta}{d\sigma} = -\frac{2}{b\sigma'_f} \left(\frac{\sigma}{\sigma'_f} \right)^{-(1+b)/b} \quad \sigma > 0, \sigma \text{ increasing} \quad (21)$$

In the time domain the damage rate D will be given as

$$\dot{D}(t) = \frac{d\delta}{d\sigma} \frac{d\sigma}{dt} = -\frac{2}{b\sigma'_f} \left(\frac{\sigma}{\sigma'_f} \right)^{-(1+b)/b} \frac{d\sigma}{dt} \quad \sigma > 0, \sigma \text{ increasing} \quad (22)$$

and the accumulated damage will be

$$D(t) = \int_0^t -\frac{2}{b\sigma'_f} \left(\frac{\sigma}{\sigma'_f} \right)^{-(1+b)/b} \frac{d\sigma}{dt} dt \quad \sigma > 0, \sigma \text{ increasing} \quad (23)$$

Extension to the more general case equation (20) is obvious.

It is also noted that $D(t)$ is a monotonically increasing function of time.

Strain Strain-Rate Continuum Damage Model

The Damage Equation (eq. (18)) in terms of stress is based on an analysis of a hysteresis cycle, under the assumptions of zero mean stress and that all the damage occurs during the extensive (tensile) part of the loop ($\sigma > 0$ and σ increasing). Extension to compressive damage is obvious and leads to symmetric terms with fractional multipliers (eq. (20)).

The results are believed to be correct so long as hysteresis cycles (or similar load) are being analyzed. However, consider, the loading case shown in figure 7. In this loading scenario the last segment, $A \rightarrow B$, completes a hysteresis loop B, E, F, A, B . But shortly into the return (Point C) the loading is again increased. A profile similar to $C \rightarrow D$ will be experienced. Note that most of $C \rightarrow D$ is elastic. After point D is reached, strong plastic strain will be again be experienced.

Integration of equation (18) will predict the same damage for $C \rightarrow D$ as $A \rightarrow B$, since the stress levels and changes are the same. Use of equation (18) for $A \rightarrow B$ will yield a correct damage estimate. However, it is believed that its use on leg $C \rightarrow D$ will be overly conservative since the plastic deformation is relatively much smaller. It is further believed that a damage rate equation based on plastic strain and strain rate will more accurately predict the damage rates on both $A \rightarrow B$ and $C \rightarrow D$, and will be more generally applicable.

The derivation of the damage model in terms of plastic strain and strain rate will be derived for the tensile damage only case and is based therefore on equation (18a).

Consider a hysteresis loop (fig. 8) of amplitude σ_a, ϵ_a . For the case described only the lower curve FGC need be considered. The equation for this curve, reference 6 is given as

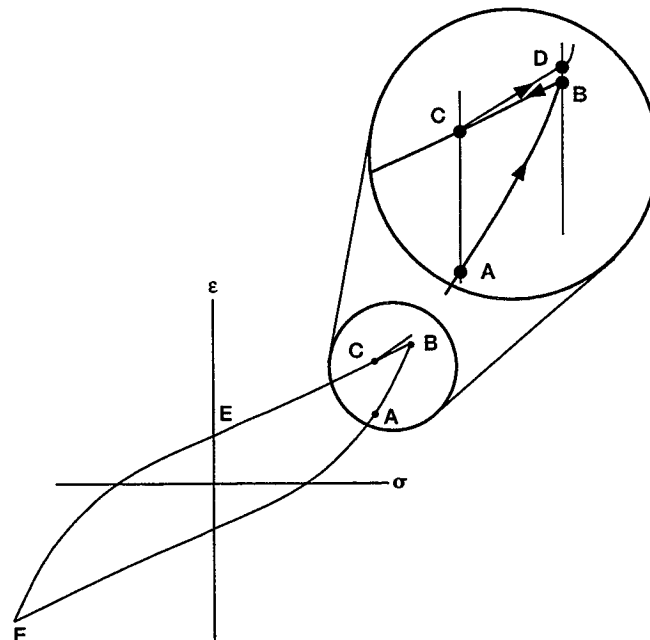


Figure 7.—Illustrative loading case.

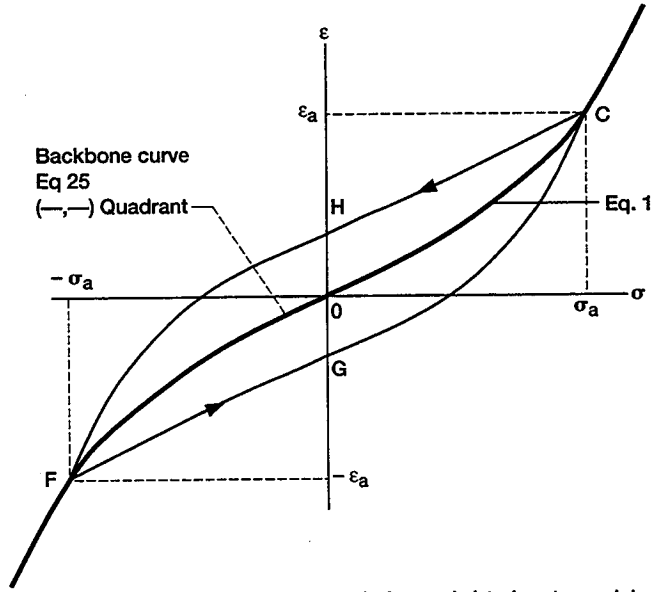


Figure 8.—Reference hysteresis cycle for strain/strain rate model.

$$\frac{\varepsilon - \varepsilon_r}{2} = \frac{\sigma - \sigma_r}{2E} + \left(\frac{\sigma - \sigma_r}{2A} \right)^{1/s} \quad (24)$$

where σ and ε are the stress and strain respectively on FGC and $(\sigma_r, \varepsilon_r)$ are the coordinates of the previous strain reversal (point F here). The curve for the locus of reversal points (for $(-, -)$ quadrant) is

$$\varepsilon_a = -\frac{\sigma_a}{E} - \left(\frac{\sigma_a}{A} \right)^{1/s} \quad (25)$$

Letting $\varepsilon_r = -\varepsilon_a$ and $\sigma_r = -\sigma_a$ in equation (24) and replacing ε_a by equation (25) gives

$$\varepsilon = \varepsilon_p + \varepsilon_e = \frac{\sigma}{E} - \left(\frac{\sigma_a}{A} \right)^{1/s} + 2 \left(\frac{\sigma + \sigma_a}{2A} \right)^{1/s} \quad \text{for FGC} \quad (26)$$

where ε_p is the plastic strain component and ε_e is the elastic strain component (σ/E). Considering only the plastic strain component gives

$$\varepsilon_p = 2 \left(\frac{\sigma + \sigma_a}{2A} \right)^{1/s} - \left(\frac{\sigma_a}{A} \right)^{1/s} \quad \text{for FGC} \quad (27)$$

Now, differentiating with respect to σ yields the plastic strain rate as

$$\varepsilon'_p = \frac{d\varepsilon_p}{d\sigma} = \frac{1}{As} \left(\frac{\sigma + \sigma_a}{2A} \right)^{(1-s)/s} \quad \text{for FGC} \quad (28)$$

Solving for σ_a from this equation gives

$$\sigma_a = 2A \left(A s \epsilon'_p \right)^{s/(1-s)} - \sigma \quad (29)$$

This equation indicates that given a family of zero mean stress hysteresis curves, of various amplitudes, the particular curve corresponding to stress amplitude, σ_a , can be identified knowing the plastic strain slope ϵ'_p and the stress level.

Now σ_a can be replaced in equation (27) by the expression of equation (29) and solving for σ gives

$$\sigma = 2A \left(A s \epsilon'_p \right)^{s/(1-s)} - A \left[2 \left(A s \epsilon'_p \right)^{1/(1-s)} - \epsilon_p \right]^s \quad (30)$$

This equation relates the stress level to the plastic strain rate and strain over curve FGC. The relationship holds regardless of cycle stress amplitude σ_a . The damage rate $\delta'(\sigma)$ in equation (18) can now be expressed in terms of ϵ_p and ϵ'_p by substituting equation (30) into equation (18), thus

$$\delta'(\epsilon_p, \epsilon'_p) = -\frac{2}{b\sigma'_f} \left\{ \frac{2A \left(A s \epsilon'_p \right)^{s/(1-s)} - A \left[2 \left(A s \epsilon'_p \right)^{1/(1-s)} - \epsilon_p \right]^s}{\sigma'_f} \right\}^{-(1+b)/b} \quad (31)$$

$\sigma > 0$, σ increasing

This is the basic result of this section, it applies to the tensile stress only case. Extension to the compressive damage cases requires consideration of the curve CHF in figure 8. Again reference 6 gives the equation for this curve as

$$\frac{\epsilon_r - \epsilon}{2} = \frac{\sigma_r - \sigma}{2E} + \left(\frac{\sigma_r - \sigma}{2A} \right)^{1/s} \quad (32)$$

With $\sigma_r = \sigma_a$ and $\epsilon_r = \epsilon_a = \sigma_a/E + (\sigma_a/A)^{1/s}$ the plastic strain for CHF becomes

$$\epsilon_p = \left(\frac{\sigma_a}{A} \right)^{1/s} - 2 \left(\frac{\sigma_a - \sigma}{2A} \right)^{1/s} \quad (33)$$

and

$$\epsilon'_p = \frac{1}{As} \left(\frac{\sigma_a - \sigma}{2A} \right)^{(1-s)/s} \quad \text{for CHF} \quad (34)$$

Following a derivation similar to that above and using equation (19) as the basis gives

$$\delta'(\epsilon_p, \epsilon'_p) = -\frac{2}{b\sigma'_f} \left\{ \frac{\left[2A(As\epsilon'_p)^{s/(1-s)} + A\left[\epsilon_p + 2(As\epsilon'_p)^{1/(1-s)} \right]^s \right]^{-(1+b)/b}}{\sigma'_f} \right\} \quad (35)$$

$\sigma < 0$, σ decreasing

as the compressive damage only expression. Extension to the combined tensile compressive damage case of equation merely requires the multiplication of equations (31) and (35) by k and $(1 - k)$ respectively.

The discussion that follows shows how $\delta'(\epsilon_p, \epsilon'_p)$ can be determined in application. It will be assumed stress, σ , and strain, ϵ , measurements or estimates are available at the critical load (damage) point(s) of the structure. It is desired to estimate $\epsilon_p(t)$ and $\epsilon'_p(t)$ at such a point. The estimate(s) are based on the graph of figure 9. The Elastic Modulus (E) is assumed to be known and constant. During elastic straining (loading)

$$\epsilon_e = \frac{\sigma}{E}$$

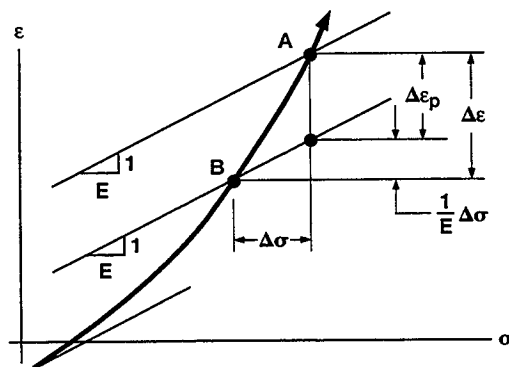
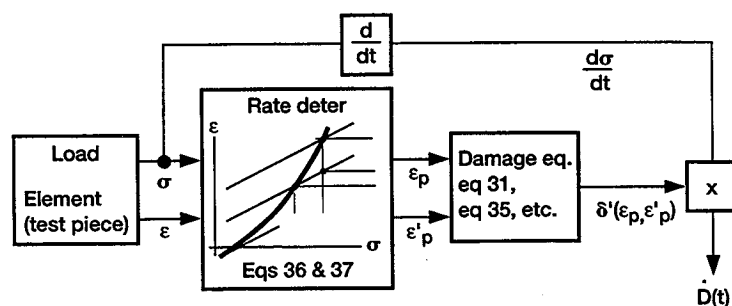


Figure 9.—Damage computation based on plastic strain and plastic strain rate.

Then the plastic strain at point A, is given by

$$\varepsilon_{pA} = \varepsilon_A - \frac{\sigma_A}{E} \quad (36)$$

The plastic strain rate ε'_{pA} is determined based on a small step from point B, thus:

$$\varepsilon'_p = \left. \frac{d\varepsilon_p}{d\sigma} \right|_A \approx \frac{\Delta\varepsilon_{pA}}{\Delta\sigma_A} = \frac{\varepsilon_A - \varepsilon_B - \frac{1}{E}(\sigma_A - \sigma_B)}{\sigma_A - \sigma_B} \quad (37a)$$

or

$$\varepsilon'_{pA} \approx \frac{\varepsilon_A - \varepsilon_B}{\sigma_A - \sigma_B} - \frac{1}{E} \quad (37b)$$

This form is valid for both legs of the hysteresis cycle so long as B is taken as the trailing point.

Now of course equations (31) and (35) are converted to time dependent forms as was done in equation (22) i.e.,

$$\dot{D}(t) = \frac{d\delta}{d\sigma} \frac{d\sigma}{dt} = \delta'(\varepsilon_p, \varepsilon'_p) \frac{d\sigma}{dt} \quad (38)$$

Non-Zero Mean Stress Continuum Damage Model

The previous sections have suggested continuous models based on the case of zero mean stress. It is important to examine the effect of mean stress in this regard. While many expressions have been generated in the cyclic damage format for the effect of mean stress, the following equation (ref. 7) will be used to attempt to generate a continuum nonzero mean stress damage model:

$$\varepsilon_a = \frac{\sigma'_f - \sigma_m}{E} (2N_f)^b + \varepsilon'_f \left(1 - \frac{\sigma_m}{\sigma'_f} \right)^{c/b} (2N_f)^c \quad (39)$$

In this expression σ_m represents the mean cyclic stress. Assuming the cyclic stress-strain behavior of the material is not altered by mean stress then

$$\varepsilon_a = \frac{\sigma_a}{E} + \left(\frac{\sigma_a}{A} \right)^{1/s} \quad (40)$$

and $N_f = 1/\delta_{cyc}$ may be used to express equation (39) in terms of stress amplitude and damage per cycle giving

$$\frac{\sigma_a}{E} + \left(\frac{\sigma_a}{A} \right)^{1/s} = \frac{\sigma'_f - \sigma_m}{E} \left(\frac{\delta_{cyc}}{2} \right)^{-b} + \varepsilon'_f \left(1 - \frac{\sigma_m}{\sigma'_f} \right)^{c/b} \left(\frac{\delta_{cyc}}{2} \right)^{-c} \quad (41)$$

Equating the elastic parts and solving for δ_{cyc} yields

$$\delta_{cyc_e} = 2 \left(\frac{\sigma_a}{\sigma'_f - \sigma_m} \right)^{-1/b} \quad (42)$$

Equating the plastic parts of equation (41) gives

$$\left(\frac{\sigma_a}{A} \right)^{1/s} = \epsilon'_f \left(1 - \frac{\sigma_m}{\sigma'_f} \right)^{c/b} \left(\frac{\delta_{cyc_p}}{2} \right)^{-c} \quad (43)$$

or

$$\left(\frac{\delta_{cyc_p}}{2} \right)^{-c} = \frac{1}{\epsilon'_f} \left(\frac{\sigma_a}{A} \right)^{1/s} \left(\frac{\sigma'_f - \sigma_m}{\sigma'_f} \right)^{-c/b} \quad (44)$$

Using the material relationships, equations (9) and (10) and after some algebraic manipulation, solving for δ_{cyc_p} yields amazingly

$$\delta_{cyc_p} = 2 \left(\frac{\sigma_a}{\sigma'_f - \sigma_m} \right)^{-1/b} \quad (45)$$

The logic proceeds as in the zero mean stress case, i.e., since

$$\delta_{cyc} = 2 \left(\frac{\sigma_a}{\sigma'_f - \sigma_m} \right)^{-1/b} \quad (46)$$

satisfies both elastic and plastic terms of equation (41) it is a solution of equation (41) and represents a simplified mean stress cyclic damage law. The value of this form (eq. (46)) over that of equations (41) or (39) is that it may be explicitly solved for any quantity. Figure 10 shows the character of equation (46) for various levels of damage/cycle, δ_{cyc} .

With the availability of the explicit form (eq. (46)) a mean stress condition continuum damage model formulation may be attempted.

The case where all the cyclic damage occurs only between σ_m and $\sigma_m + \sigma_a$ on the tensile leg (fig. 11) is considered. The problem is to determine a damage rate $\delta'(\sigma)$ over this domain such that:

$$\int_{\sigma_m}^{\sigma_m + \sigma_a} \delta'(\sigma) d\sigma = \delta_{cyc} = 2 \left(\frac{\sigma_a}{\sigma'_f - \sigma_m} \right)^{-1/b} \quad (47)$$

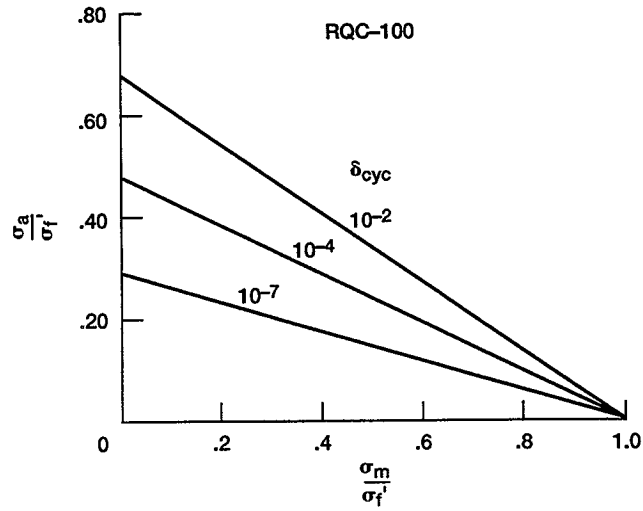


Figure 10.—Effects of mean stress and stress amplitude on damage per cycle, δ_{cyc} , for RQC-100 steel.

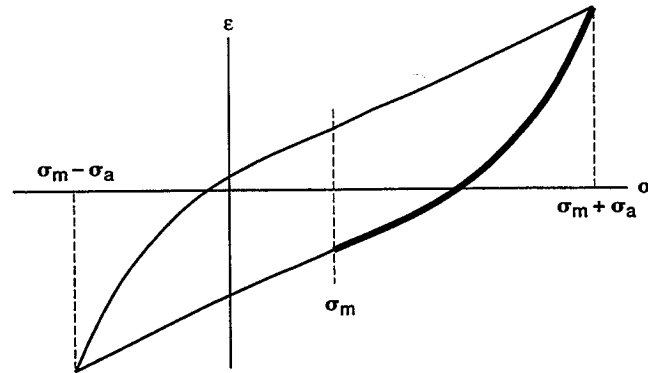


Figure 11.—Assumed damage location for tensile side only mean stress damage model.

Now since

$$\int_a^x f(y) dy = \int_0^{x-a} f(y+a) dy$$

the problem can be reformulated as

$$\int_0^{\sigma_a} \delta'(\sigma + \sigma_m) d\sigma = 2 \left(\frac{\sigma_a}{\sigma'_f - \sigma_m} \right)^{-1/b} \quad (48)$$

Then differentiating the right-hand side of equation (48) gives

$$\delta'(\sigma + \sigma_m) = -\frac{2}{b} \left(\frac{1}{\sigma'_f - \sigma_m} \right)^{-1/b} (\sigma)^{-(1/b)-1}$$

and the desired integrand then is given by

$$\delta'(\sigma) = -\frac{2}{b} \left(\frac{1}{\sigma'_f - \sigma_m} \right)^{-1/b} (\sigma - \sigma_m)^{-(1+b)/b}$$

for $\sigma'_f \geq \sigma \geq \sigma_m \geq 0$, σ increasing (49)

This then (eq. (49)), is the desired damage rate for a hysteresis cycle with a mean stress condition. The hope prior to starting this part of the analysis was that this expression would be found to be independent of σ_m so that a "universal" stress based continuum form would be obtained, this unfortunately was not the case.

This equation (eq. (49)) parallels equation (18) and can be seen to reduce to it when $\sigma_m = 0$. Further, if it assumed that damage occurs equally in tension increasing and compression increasing modes, then

$$\delta'(\sigma) = -\frac{1}{b} \left(\frac{1}{\sigma'_f - \sigma_m} \right)^{-1/b} \left(|\sigma - \sigma_m| \right)^{-(1+b)/b} \quad (50)$$

may be used, paralleling equation (19). And for unequal damage on the tensile and compressive legs for the mean stress case

$$\delta'(\sigma) = \begin{cases} -2 \frac{k}{b} \left(\frac{1}{\sigma'_f - \sigma_m} \right)^{-1/b} \left(|\sigma - \sigma_m| \right)^{-(1+b)/b} & \sigma > \sigma_m, \sigma \text{ increasing} \\ -2 \frac{(1-k)}{b} \left(\frac{1}{\sigma'_f - \sigma_m} \right)^{-1/b} \left(|\sigma - \sigma_m| \right)^{-(1+b)/b} & \sigma < \sigma_m, \sigma \text{ decreasing} \end{cases} \quad (51)$$

and equation (51) parallels equation (20).

The effect of mean stress level on damage rate for RQC-100 steel is shown in figure 12 for the tensile only damage assumption (eq. (49)). It is very important to note here that for stress levels less than 0.925 the zero mean stress damage rate is greater than all non zero mean stress cases (for $\sigma_m = 0$). That is, the simple zero mean stress damage law of equation (18), is conservative in predicting damage rate at these stress levels (with mean stress). This suggests that it may be feasible to use the envelope (maximum) damage curve as a conservative damage law for practical Life Extending Control applications.

For $\sigma_m > 0$, the maximum damage curve at a given (constant) stress level, is determined by setting the derivative of $\delta'(\sigma)$ in equation (49) to zero, thus

$$\frac{d\delta'}{d\sigma_m} = \frac{2}{b^2} (\sigma - \sigma_m)^{-(1+b)/b} (\sigma'_f - \sigma_m)^{-(1+b)/b} - \frac{2(1+b)}{b^2} (\sigma'_f - \sigma_m)^{1/b} (\sigma - \sigma_m)^{-(1+2b)/b} = 0 \quad (52)$$

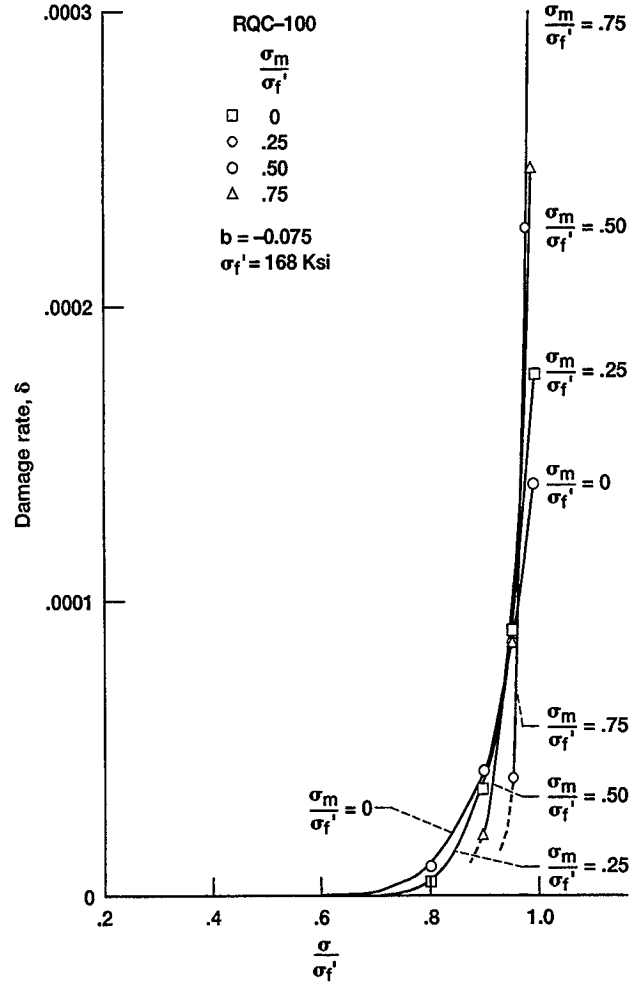


Figure 12.—Damage rate verses normalized stress level with $\sigma_m/\sigma_f' = 0, .25, .50, .75$.

After considerable algebra, this yields the condition

$$\frac{\sigma_m}{\sigma_f'} = -\frac{1}{b} \frac{\sigma}{\sigma_f'} + \frac{1+b}{b} \quad \text{for } \sigma_f' > \sigma_m > 0 \quad (53)$$

Substituting this results into equation (49) and after considerable simplification

$$\delta'(\sigma)_{max} = \frac{2(1+b)^{-(1+b)/b}}{\sigma_f' - \sigma} \quad \text{for } \sigma_f' > \sigma_m > 0 \quad (54)$$

In words; the maximum damage rate is inversely proportional to the distance of the stress from σ_f' . It can be shown from equation (53), with $\sigma_m/\sigma_f' = 0$ that equation (54) only applies for

$$\frac{\sigma}{\sigma_f'} \geq 1 + b \quad (55)$$

Thus for RQC-100, $1 + b = 0.925$, and equation (54) is seen to determine δ'_{max} for $\sigma/\sigma'_f \geq 0.925$ while below that level the zero mean stress equation (18) dominates. Extension, of the mean stress based damage laws to the time domain follows that shown for equations (22) and (23) with obvious changes in $d\delta/d\sigma$. Note, if σ_m is allowed to be negative damage rates can exceed the zero mean stress damage prediction.

Concluding Remarks

This effort seeks to create a continuum fatigue damage model. This initial effort attempts to mathematically convert the classic cycle based damage results as represented by the Local Strain Approach into a continuum model. The results achieved to date have been encouraging. Under the assumption of zero mean stress it has been shown that the continuum damage rate can be expressed as a highly nonlinear function of the instantaneous stress (eqs. (18) to (22)). These continuum rates are compatible with hysteretic damage. In the process of achieving these results explicit simplified forms of the cyclic damage laws have been developed (eqs. (15) and (46)). Also time domain implementations have been derived (eqs. (22) and (23)). A continuum fatigue damage model in terms of plastic strain and plastic strain rate has been shown to be equivalent to the stress based model for zero mean stress hysteretic damage but is believed to be superior for general application. This has not been validated.

The case of non-zero mean stress is more difficult both conceptually and analytically. Here also, an explicit simplified form of the cyclic damage law (eq. (46)) has been developed. Based on this explicit form, stress level based damage rate expressions (eqs. (49) to (51)) have been derived under various assumptions. The assumptions center around broad questions of where in the cycle damage occurs.

Initial comparisons between the positive mean stress case and the zero mean stress case have shown that for stress levels up to 92.5 percent of σ'_f that the zero mean stress continuum model yields conservative results (i.e., greater damage). Thus for Life Extending (or Damage Mitigating) Control it may be applied to most practical situations.

Left open is the question of the nonlinear damage effects, namely the effect of accumulated damage on damage rate. While not reported yet, some progress has been made in this area with the availability of the simplified expressions discussed above. What is needed are appropriate cyclic data sets showing variations in stress amplitude versus cycles, for constant strain amplitude testing, to allow calibration of the effect. Further research effort is also needed to create plastic strain/strain-rate damage model for the mean stress case. Further, study of the relationship between this model and that for the zero mean stress should be done.

Finally experimental studies are required to screen broadly where the intracycle damage occurs. Such studies are now being started. Availability of such data will determine which assumptions of the analysis (i.e., tension damage only, etc.) apply. In the longer run further experimental validation of the proposed continuum models will also be required.

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